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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

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|--------------|------------------------------|
| Appl. No. | : 09/441,119 |
| Applicant | : Oliver L. Richards, et al. |
| Filed | : November 17, 1999 |
| T.C./A.U. | : 2611 |
| Examiner | : Usha Raman |
| Docket No. | : ALLEG-017PUS |
| Customer No. | : 022494 |

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26 April 2004
Date of Signature
and Mail Deposit

By: Judith C. Crowley
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Mail Stop AF
Commissioner for Patents
P.O. Box 1450
Alexandria, VA 22313-1450

Dear Sir:

SUBSTITUTE DECLARATION UNDER 37 CFR §1.131

1. I, Paul M. Greenland, am a co-inventor of a U.S. Patent Application entitled "Low Noise Block Supply and Control Voltage Regulator" now pending before the U. S. Patent Office as Application No. 09/441,119.
2. Prior to December 1998, I, along with co-inventor Oliver L Richards, conceived of the invention described in U. S. Patent Application No. 09/441,119, as evidenced by a

schematic captioned "LNB BUCK/BOOST PROPOSAL" and attached hereto as Exhibit A.

3. Following conception, I worked on developing a product incorporating the technology described in U. S. Patent Application No. 09/441,119, as evidenced by a schematic captioned "LNB BUCK REGULATOR PROPOSAL," dated 31 March 1999, and attached hereto as Exhibit B as well as a Product Preview datasheet for the 8284 Product of Allegro Microsystems, Inc. dated 19 July 1999 and attached hereto as Exhibit C.

4. The subject patent application was filed in the U.S. Patent Office on November 17, 1999.

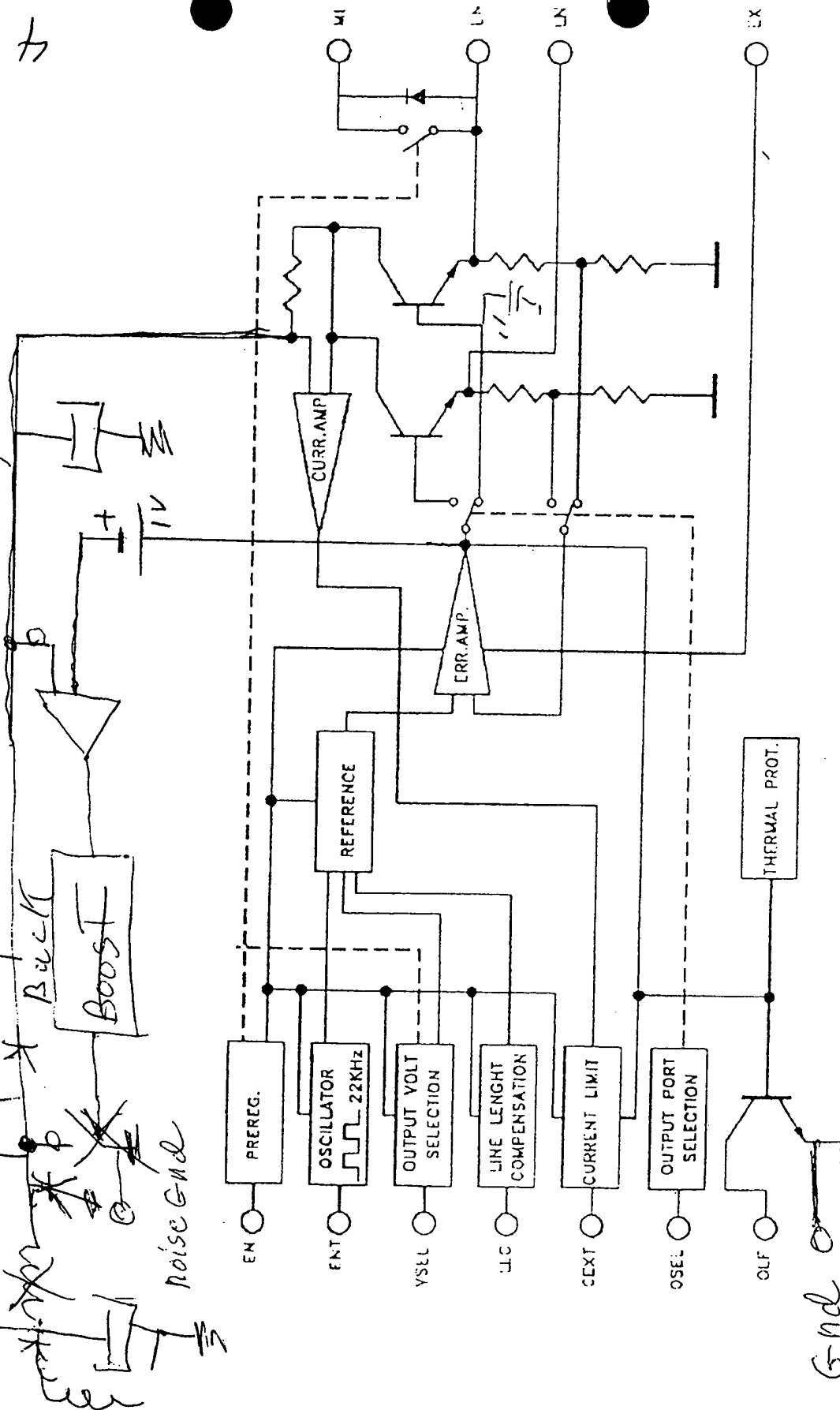
5. All of the statements made herein are of my own knowledge and are true, these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment or both, under § 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application and any patent issuing thereon, or any patent to which this verified statement is applied.

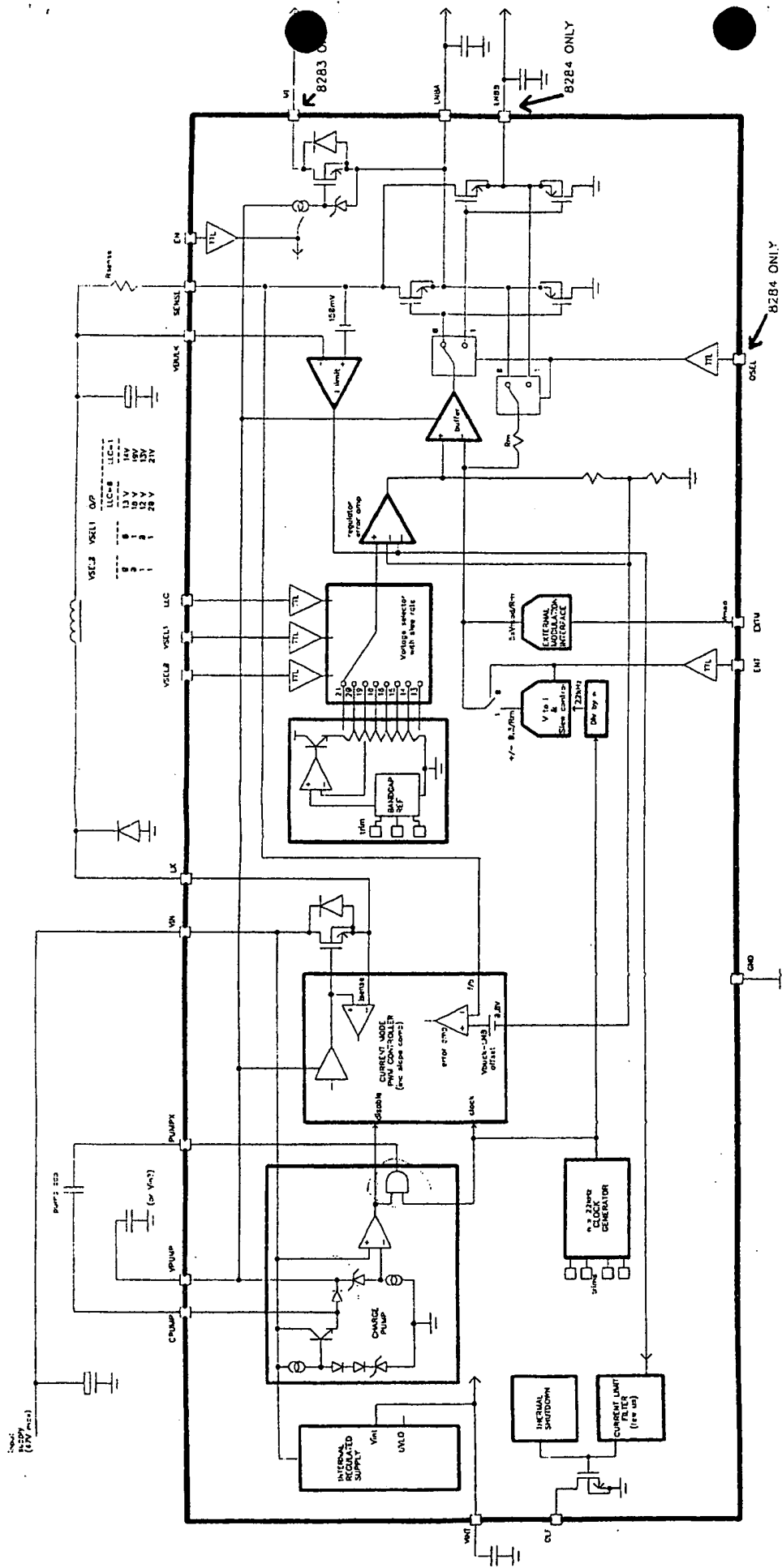
4/19/04
Date of Signature

By: Paul Greenland
Paul M. Greenland

LN B Boost Proposal
Buck

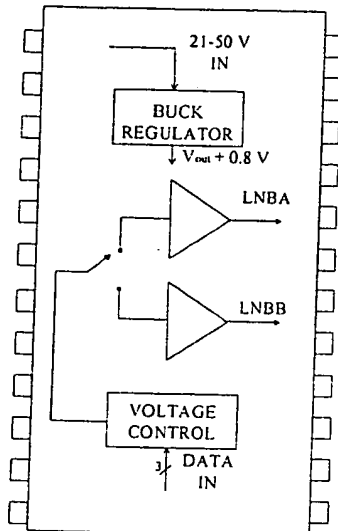
(3.7, 15.7, 19.7 20.7 Volts)





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Interim Data Sheet



Two Output LNB Supply and Control Voltage Regulator

- Complete interface for two LNBs remote supply and control
- LNB selection and stand-by function
- Built-in tone oscillator factory trimmed to 22 kHz facilitates DiSEqC™ encoding
- Full modulation with no load
- Tracking switch-mode power converter for lowest dissipation
- Externally adjustable short-circuit protection
- LNB short-circuit protection and diagnostics
- Auxiliary modulation input
- Cable length compensation
- Internal over temperature protection
- Reverse current protection

Intended for analog and digital satellite receivers, the low noise block converter regulator (LNBR) is a monolithic linear and switching voltage regulator, specifically designed to provide the power and the interface signals to the LNB downconverter via the coaxial cable. Because most satellite receivers have two antenna ports, the output voltage of the regulator is available at one of two logic-selectable output terminals (LNBA, LNBB). If the device is in stand-by mode (EN terminal LOW), both regulator outputs are disabled. This is to allow the antenna downconverters to be supplied and controlled by other satellite receivers sharing the same coaxial cable. In this mode the device will limit reverse current to 3 mA.

ABSOLUTE MAXIMUM RATINGS

| | |
|---|--------------------|
| DC Input voltage..... | 50 V |
| Output Current | Internally limited |
| Logic Input Voltage..... | -0.5 to 7 V |
| Storage temperature range..... | -40 to 150°C |
| Operating Junction Temperature Range..... | -40 to 150°C |

The regulator outputs are set to 12, 13, 18, or 20 volts by the VSEL terminals. Additionally, it is possible to increase by 1 V the selected voltage to compensate the voltage drop in the coaxial cable (LLC terminal HIGH).

Cont....

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The LNBR is a combination of a tracking switching regulator and low-noise linear regulators. Logic inputs (VSEL0, VSEL1 and LLC) select the desired output voltage. A tracking current-mode buck converter provides the linear regulator input voltage that is set to the output voltage plus typically 0.8 volt. This maintains constant voltage drop across the linear regulators while permitting adequate voltage range for tone injection.

The ENT (Tone Enable) terminal activates the internal tone signal modulating the dc output with a ± 0.3 V, 22 kHz symmetrical waveform. The internal oscillator is factory trimmed to provide a tone of $22 \text{ kHz} \pm 2 \text{ kHz}$. No further adjustment is required. The internal oscillator operates the buck converter at 16 times the tone frequency.

Burst coding of the 22 kHz tone can be accomplished, due to the fast response of the ENT input and rapid tone response. This allows implementation of the DiSEqC™ protocols.

To improve design flexibility and to allow implementation of proposed LNB remote control standards, an analog modulation input terminal is available (EXTM). An appropriate dc blocking capacitor must be used to couple the modulating signal source to the EXTM terminal. If external modulation is not used, the EXTM terminal can be left open.

The output linear regulators will sink and source current. This feature allows full modulation capability into capacitive loads as high as 250 nF.

The programmed output voltage rise and fall times can be set by an internal 50 k Ω resistor and an external capacitor located on the TCAP terminal. Although any value of capacitor is permitted, practical values are typically 1 nF to 20 nF. This feature only affects the turn on and programmed voltage rise and fall times. Modulation is unaffected by the choice of TCAP. This terminal can be left open if voltage rise and fall time control is not required.

Two terminals are dedicated to the over current protection/monitoring: SENSE and OLF. The LNB output is current limited. The short-circuit protection threshold is set by the value of an external resistor, R_{sense} . $R_{sense} = 0.15/I_{max}$ where I_{max} is the desired current limit. The minimum safe value for R_{sense} is 0.22 ohm

In operation the short-circuit protection produces current fold-back at the input due to the tracking converter. If the output is shorted the linear regulator will limit the output current to I_{max} . The tracking converter will maintain a constant voltage drop of 0.8 volts across the linear regulator. This condition results in $(I_{max}) \cdot (0.8 \text{ volts})$ or typically 550 mW dissipation. Short-circuit or thermal shutdown activation will cause the OLF terminal, an open-drain diagnostic output flag, to go LOW.

The device is packaged in a 24 DIP or an SOIC power-tab package.

Thermal resistance: DIP $R_{\theta JA}=40^{\circ}\text{C/W}$, $R_{\theta JT}=6^{\circ}\text{C/W}$, SOIC $R_{\theta JA}=55^{\circ}\text{C/W}$, $R_{\theta JT}=6^{\circ}\text{C/W}$

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Terminal Configuration

| Symbol | Terminal | Function |
|------------|----------|--|
| VINT | | Bypass capacitor for internal voltage reference |
| CPUMP | | High side of charge-pump cap |
| EN | | Logic input: enables switcher and outputs |
| ENT | | Logic input: enable internal modulation |
| EXTM | | External modulation input |
| GND | | Ground |
| VBULK | | Tracking supply voltage to linear regulators |
| LLC | | Logic input: increases output voltage by 1 V for line length |
| Voa | | LNBA output voltage A |
| Vob | | LNBB output voltage B |
| LX | | Inductor drive point |
| SENSE | | Current limit setup resistor |
| OLF | | Overload flag output |
| OSEL | | Logic input: selects between LNB, A or B |
| VIN or Vcc | | Supply input voltage (range VLNB+2.5 V to 47 V) |
| VPUMP | | Gate supply voltage for high side drivers |
| PUMPX | | Charge-pump drive |
| TCAP | | Capacitor for setting the rise and fall time of the outputs |
| VSEL0 | | Logic input: output voltage select |
| VSEL1 | | Logic input: output voltage select |

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Electrical Characteristics for LNBR Series ($T_A = 25^\circ\text{C}$, ENT=L, EN=H, LLC=L, $V_{IN}=24\text{ V}$, $I_{out}=50\text{ mA}$ (unless otherwise specified)).

| Symbol | Parameter | Test Conditions | Min. | Typ. | Max | Unit |
|-------------------|--|--|-----------|------------|----------|------------------|
| V_{IN} | V_{CC1} Supply Voltage | $I_O=600\text{ mA}$, VSEL0=L, VSEL1=L, LLC=L | $2.5+V_O$ | | 47 | V |
| V_{O1} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=L, VSEL1=H, LLC=L | 17.3 | 18 | 18.7 | V |
| V_{O2} | Output Voltage | $I_O=600\text{ mA}$, SEL0=L, VSEL1=H, LLC=H | | 19 | | V |
| V_{O1} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=L, VSEL1=L, LLC=L | 12.5 | 13 | 13.5 | V |
| V_{O1} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=L, VSEL1=L, LLC=H | | 14 | | V |
| V_{O2} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=H, VSEL1=H, LLC=L | | 20 | | V |
| V_{O2} | Output Voltage | $I_O=600\text{ mA}$, SEL0=H, VSEL1=H, LLC=H | | 21 | | V |
| V_{O2} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=H, VSEL1=L, LLC=L | | 12 | | V |
| V_{O2} | Output Voltage | $I_O=600\text{ mA}$, VSEL0=H, VSEL1=L, LLC=H | | 13 | | V |
| ΔV_O | Line Regulation | $V_O=13\text{ V}$, $V_{IN}=16\text{ to }40\text{ V}$ $V_O=18\text{ V}$, $V_{IN}=21\text{ to }40\text{ V}$ | | 4.0 4.0 | 40 40 | mV mV |
| ΔV_O | Load Regulation | $V_O=13\text{ or }18\text{ V}$, $I_O=50\text{ to }600\text{ mA}$ | | 80 | 180 | mV |
| SVR | Supply Voltage Rejection | $f_{AC}=100\text{ Hz}$ | | 45 | | dB |
| I_{MAX} | Output Current Limiting | $R_{sense}=0.22\text{ ohm}$ | 630 | 680 | 730 | mA |
| f_{TONE} | Tone Frequency | ENT=H | 20 | 22 | 24 | kHz |
| a_{TONE} | Tone Amplitude | ENT=H | 0.55 | 0.68 | 0.8 | V _{pp} |
| d_{TONE} | Tone duty cycle | ENT=H | 40 | 50 | 60 | % |
| t_R, t_F | Tone rise or fall time | ENT=H | 5.0 | 10 | 15 | μs |
| g_{EXTM} | External modulation gain | $\Delta V_O / \Delta V_{EXTM}$, $f=10\text{ Hz to }40\text{ kHz}$ | | 1.0 | | V/V |
| V_{EXTM} | External modulation input voltage | AC coupling | | | 0.8 | V _{pp} |
| Z_{EXTM} | External modulation input impedance | $f=10\text{ Hz to }40\text{ kHz}$ | | 5 | | k Ω |
| V_{OL} | Overload flag terminal logic low | $I_{OL}=8.0\text{ mA}$ | | 0.28 | | V |
| I_{OZ} | Overload flag terminal OFF state leakage current | $V_{OH}=6.0\text{ V}$ | | < 1.0 | | μA |
| V_{IL} | Control input terminal logic low | | | | 0.8 | V |
| V_{IH} | Control input terminal logic high | | 2.0 | | | V |
| I_{IH} | Control terminals input current | $V_{IH}=5\text{ V}$ | | < 1.0 | | μA |
| I_{CC} | Supply current | Outputs disabled (EN=L) | | .5 | | mA |
| I_{CC} | Supply current | ENT=H, $I_{OUT}=600\text{ mA}$, $V_O=13$ | | 382 | | mA |
| I_{OBK} | Output reverse current | EN=L, $V_{LNBA}=V_{LNBB}=18\text{ V}$ $V_{IN1}=V_{IN2}=22\text{ V}$ or floating | | 1.0 | | mA |
| T_{SHDN} | Thermal shutdown threshold | | | 165 | | $^\circ\text{C}$ |
| ΔV_{BUCK} | Linear regulator voltage drop | $V_{BULK} - V_O$ | | 0.8 | | V |
| f_o | Switching frequency | $f_{TONE} * 16$ | 320 | 352 | 384 | kHz |

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Truth Tables

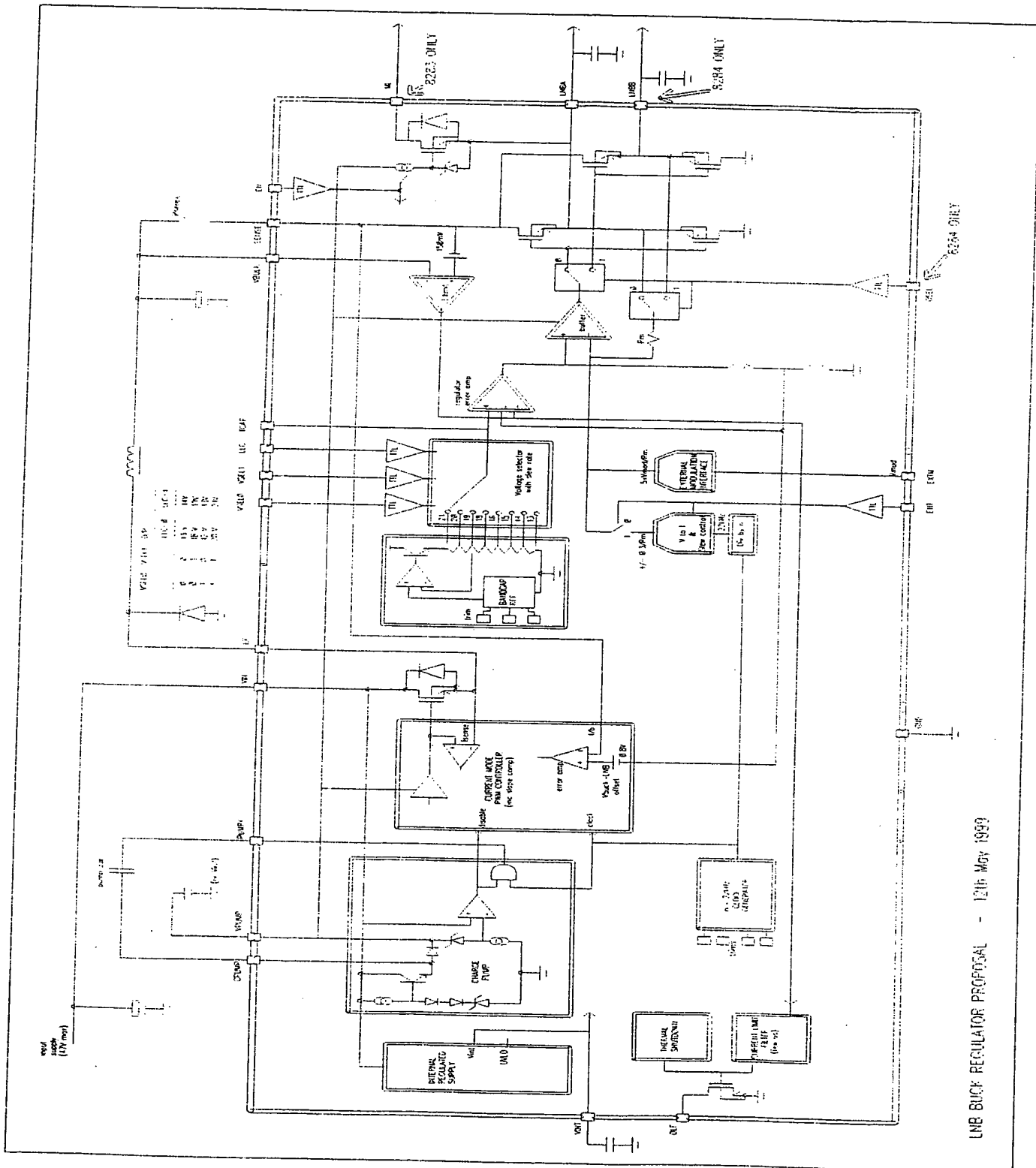
| Control I/O | Terminal Name | L | H |
|-------------|---------------|--|---|
| OUT | OLF | $I_{out} > I_{max}$ or $T_j > 165^{\circ}\text{C}$ | $I_{out} < I_{max}$ and $T_j < 130^{\circ}\text{C}$ |
| IN | ENT | 22 kHz tone OFF | 22 kHz tone ON |

| SEL | VSEL0 | VSEL1 | LLC | VLNBA (typ.) | VLNBB (typ.) |
|-----|-------|-------|-----|--------------|--------------|
| L | L | L | L | 13 V | Low |
| L | L | H | L | 18 V | Low |
| L | L | L | H | 14 V | Low |
| L | L | H | H | 19 V | Low |
| H | L | L | L | Low | 13 V |
| H | L | H | L | Low | 18 V |
| H | L | L | H | Low | 14 V |
| H | L | H | H | Low | 19 V |
| L | H | L | L | 12 V | Low |
| L | H | H | L | 20 V | Low |
| L | H | L | H | 13 V | Low |
| L | H | H | H | 21 V | Low |
| H | H | L | L | Low | 12 V |
| H | H | H | L | Low | 20 V |
| H | H | L | H | Low | 13 V |
| H | H | H | H | Low | 21 V |

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